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# Investigation of flocculation dynamics under changing hydrodynamic forcing on an intertidal mudflat



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#### ABSTRACT

In situ floc size and turbulent shear stress were measured together with suspended sediment concentration to investigate the floc properties under changing hydrodynamic forcing over the intertidal mudflat. A tripod system was established in the field for a period of approximately one month, including  $\sim$ 6 days of stormy conditions in the middle of the investigation period. Mean floc size exhibited strong temporal variations within a tidal cycle, and inverse relationship was found between mean floc size and shear stress. Suspended sediment concentration (SSC) can modulate the flocculation dynamics when shear stress decreases down to enhancing flocculation. Asymmetrical behaviors of floc sizes between flood and ebb phases were identified, with overall larger floc sizes in flood than in ebb tide under the same shear stresses. Floc structure showed different properties under calm and stormy conditions, and the variable fractal dimension and variable primary particle size were more convincing in simulating the variation of floc effective density with mean floc size during the storm period, which was inferred to be related to the resuspension of bed sediment as well as organic matter. A total of 110 mm bed erosion was measured during the storm, and erosion events occurred only around low water, due to the high current-wave combined bed shear stress and off-shore current. After the storm,  $\sim$  40% of the erosion recovered within one week, and the fast settling of large flocs around high water plays significant role in the deposition process, leading to  $\sim$ 60% of the recovery.

# 1. Introduction

Intertidal mudflats provide a transition zone and protective barrier between land and estuary, and they have valuable functions in terms of ecosystem development (Dyer, 1998). The overall development of a mudflat depends on the relative balance between hydrodynamics (erosion) and sediment supply (sedimentation). On a short time-scale (i.e. the tidal cycle and spring-neap cycle), hydrodynamics dominated by tidal currents and waves determine the variations of suspended sediment flux and bed level. Sedimentation usually happens during relatively calm conditions due to settling and tidal asymmetry when the sediment supply is large (Christie and Dyer, 1998; Andersen and Pejrup, 2001; Deloffre et al., 2006). Episodic energetic events like storms are important for tidal flat development and can cause significant erosion within just a few tidal cycles (Christie et al., 1999; Andersen and Pejrup, 2001). On a seasonal time-scale, the importance of biological

characteristics in modifying the initial erosion of the surface layer on a mudflat has also been found (e.g. Andersen, 2001; Uncles et al., 2003).

The transport of cohesive sediment is more complicated than non-cohesive sediment in particular due to flocculation, which is the result of simultaneously aggregation and floc break up processes (Winterwerp and Van Kesteren, 2004). Flocculation has been widely observed in varying fresh (e.g. river, lake), brackish (e.g. estuary, river deltas), and marine (e.g. open sea) waters (Droppo and Ongley, 1994; Fennessy et al., 1994; Manning and Dyer, 2007; Guo and He, 2011; Fettweis et al., 2014). Controls on flocculation processes are numerous and complex, including a number of physical and biochemical factors such as: the turbulent intensity, suspended sediment concentration (SSC), differential settling of particles, composition of primary particles, salinity, and content of organic matter and polymers, etc. (see e.g. Milligan and Hill, 1998; Manning and Dyer, 1999; Fugate and Friedrichs, 2003; Mietta et al., 2009; Verney et al., 2009; Sahin, 2014, among others).

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The conceptual diagram proposed by Dyer (1989) established that at low concentrations mean floc size first increases with shear stress at low values, followed by a decrease due to floc break up as shear stress increases, and at higher concentrations flocs are larger but more easily to be disrupted by shearing. This conceptual model was confirmed by a number of laboratory experiments and field measurements (e.g. Manning and Dyer, 1999; Kumar et al., 2010; Sahin, 2014). However, Winterwerp (1998) suggested that the long residence time of flocs required to achieve the equilibrium at low shear stress conditions  $(\sim 2-3 \text{ s}^{-1})$  could explain the increase of floc size with shear rate. In the flocculation experiments using kaolinite, Mietta et al. (2009) found that when the shear rate was  $< 35 \,\mathrm{s}^{-1}$ , flocs became smaller with shear rate decreased as deposition prevented flocs from reaching the equilibrium. Moreover, in the laboratory experiments of Milligan and Hill (1998) and field survey of Xia et al. (2004) in a microtidal estuary, they found the influence of SSC on flocculation is minor. The inconsistency in these studies may be caused by varying constitutions of flocs and environmental conditions, therefore further studies in different estuarine systems with varied hydrodynamic forcing are required to extend our knowledge of flocculation dynamics.

Investigations on mudflats have shown that sediment deposition is predominantly in the form of flocs and that the fraction of flocs decreases with the increase of bed elevation at tidal scale (e.g. Christiansen et al., 2000; Voulgaris and Meyers, 2004; Hill et al., 2013; Law et al., 2013). The settling velocity of aggregated flocs is likely orders of magnitude larger than the settling of the primary particles. Flocculation therefore leads to an increased settling flux of mud to the bed (Soulsby et al., 2013; Mehta et al., 2014) and is particularly important to the mudflat deposition (Kranck and Milligan, 1992; Manning and Dyer, 2007). Higher turbulence levels tend to resuspend sediment from the bed and disrupt flocs, while as the tidal currents approach high or low water slack, large SSC combined with low turbulent intensities encourage the aggregation of flocs and result in rapid settling (Christie et al., 1999; Milligan et al., 2007). As the effective density of a floc tends to decrease with size due to increasing water content (Fennessy et al., 1994), floc settling velocity is controlled by both floc size and structure. However, variations of floc size as well as structure over a mudflat are still partially known as both hydrodynamic forcing and SSC can be highly variable around the low water environment, especially under episodic events like storms.

Given the many uncertainties as well as partially known aspects of floc dynamics on intertidal flats, a field campaign was set up. This paper is based on the results of in situ observations of floc properties and hydrodynamics on a mudflat covering continuous stormy and calm weather conditions. We aim to further explore the time-variant floc size and structure under different forcing conditions and how these contribute to the deposition of sediment on the mudflat.

#### 2. Methodology

## 2.1. Site description

Fieldwork was conducted on the Kapellebank tidal flat, located in the lower part of the Westerschelde (Scheldt) Estuary in the Netherlands (Fig. 1a). The Scheldt estuary is a semidiurnal mesoto macro-tidal regime and extends 160 km in length. The mean tidal range at the estuary mouth fluctuates between 4.2 and 3.1 m during spring and neap tides, respectively. It increases up to about 6 m at a distance of 95 km landward, then gradually decreases to about 2.3 m. The mean SSC value in the lower Scheldt estuary (from the mouth to 58 km landward) is about 50 mg l $^{-1}$ , and the main turbidity maximum zone (TMZ) locates at roughly 60 to 100 km from the mouth, mean SSC in the TMZ can reach 200 mg l $^{-1}$  (Chen et al., 2005a). The study site Kapellebank is a semi-enclosed flat at the channel outer-bend (Fig. 1b). It is about 35 km from the mouth, where the mean tidal range is  $\sim$  4.5 m, and this area is classified as well-mixed. Bed sediment on the

Kapellebank is predominantly mud with a median grain size  $< 50 \, \mu m$  (Kuijper et al., 2004). The geometry of the tidal flat has a triangular shape with a length and width of approximately 1.8 and 0.8 km, respectively. The highest elevation of this tidal flat is about 0.6 m above the Normal Amsterdam Peil (NAP, which is approximately mean sea level). Bed level decreases towards the channel with a mild bed slope of about 3‰ (Fig. 1c). The observation site has an elevation of about  $-1.8 \, m$  and is approximately at the interface between intertidal and subtidal flats.

#### 2.2. Field measurements

Field observations were conducted in 2014, between April 28 and May 22. The time-series were interrupted twice, i.e., May 2–3 and May 13–15, when instrument batteries were exchanged. A storm occurred between the 6th and 12th of May with the maximum wind speed reached  $18~{\rm m~s^{-1}}$  at the meteorological station Vlissingen, which is on the west side of the Kapellebank (Fig. 1b). Instruments were mounted on a frame constructed with stainless steel pipes and hammered at least 1.5 m into the bed to reduce horizontal and vertical vibrations.

Near-bed 3D current velocities were measured with a 6-MHz downward-looking acoustic Doppler velocimeter (ADV, Nortek Vector) with the sampling volume (2.65 cm³) at 15 cm above the bed (cmab). ADV collected data at a sampling rate of 8 Hz continuously for 90 s, with a time interval between bursts of 10 min. Bed level variation was also measured by the ADV through recording the vertical distance between the acoustic transmitter and the bed surface with a resolution of 0.1 mm and an accuracy of  $\pm$  1 mm. Turbidity at 15 cmab was measured by an Optical Back-Scatter (OBS) 3+ sensor, which was logged by the ADV on one of its analogue channels. Wave climate at the study site was measured by a wave logger (OSSI-010-003C, Ocean Sensor Systems), which collected 4096 data points in 20 min bursts at a sampling rate of 10 Hz.

In situ floc size distributions were measured by a laser in situ scattering and transmissometry (LISST-100X, type C) instrument with the particle size spectra range between 2.5 and 500  $\mu m$ . The instrument emits laser light through a sample volume of water, then it records the energy of scattered laser and inverts it into particle size distributions based on volume concentrations at 32 logarithmically spaced ring detectors, and each detector corresponds to one size range (Agrawal and Pottsmith, 2000). Laboratory and field evaluations by Gartner et al. (2001) demonstrated that the LISST is capable of determining particle size to within  $\sim 10\%$  with increasing error as particle size increases. Numerous articles have confirmed that LISST worked reasonably well over a range of environmental conditions (e.g. Mikkelsen and Pejrup, 2001; Guo and He, 2011; Safak et al., 2013; Ramírez -Mendoza et al., 2016). The work of Chen et al. (2005b) on a mud tidal flat  $\sim$  30 km downstream from our study site with a camera showed that the largest floc size was 290  $\pm$  170 µm, indicating that the major portion of flocs in this area can be detected by the LISST-100C. The LISST was placed at 15 cmab with a sampling period of 3 min, and a 50% path reduction module was deployed to increase its sensitivity in turbid waters. For each sample period, 10 volume concentration distributions were collected over 30 s, and the averaged result was used to reduce short-time variations (Mikkelsen and Pejrup, 2001).

#### 2.3. Data processing

# 2.3.1. Hydrodynamics

Commonly there are four methods to estimate shear stress: (1) Log Profile (LP) method, (2) Reynolds stress technique, (3) Turbulent Kinetic Energy (TKE) approach, and (4) energy dissipation measurement. The TKE approach was concluded as the most consistent one (Kim et al., 2000), and it best suited to this investigation with the presence of waves because the instantaneous velocity measurements from the ADV could provide both turbulent and wave characteristics

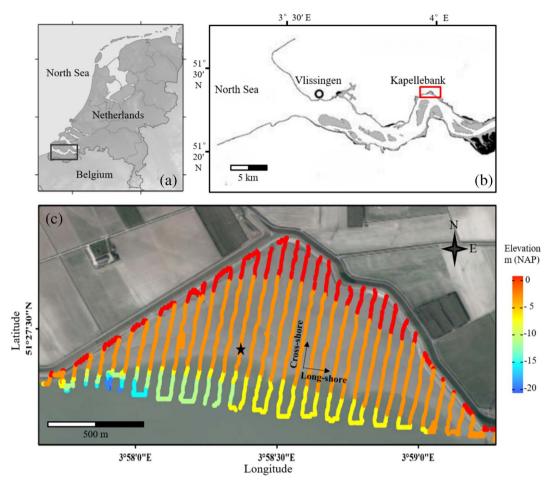


Fig. 1. (a) Geographic position of the lower Scheldt; (b) Location of the Kapellebank tidal flat; (c) The bathymetry of Kapellebank and the field observation site (marked as black star). NAP is about mean sea level.

(Verney et al., 2007). To ensure the reliability of ADV-derived data, raw velocity fluctuations were processed by removing all results with signal-to-noise (SNR) < 5 dB, and correlation < 70% as suggested by Chanson et al. (2008). The energy spectral analysis was then used to separate the turbulent kinetic energy of current-induced ( $u_c^{-2}$ ,  $v_c^{-2}$ ,  $w_c^{-2}$ ) and wave-induced ( $u_w^{-2}$ ,  $v_w^{-2}$ ,  $v_w^{-2}$ ) variances, and the influence of wave was expected to be between 0.1 and 1 Hz (Soulsby and Humphery, 1990; Verney et al., 2007). The combined bed shear stress was obtained from shear stress due to currents  $\tau_c$  and due to waves  $\tau_w$  (Wiberg and Smith, 1983):

$$\tau_{cw} = \sqrt{\tau_c^2 + \tau_w^2} \tag{1}$$

Current-induced bed shear stress was determined by the modified TKE method which uses only the vertical velocity fluctuations (Kim et al., 2000):

$$\tau_c = 0.9 \rho_w \overline{w_c^{\prime 2}} \tag{2}$$

where  $\rho_w$  is the water density (1030 kg m<sup>-3</sup>). This relationship requires the measurements be taken within the constant stress layer. As this study was conducted on an intertidal mudflat, the ADV measurement volume may have been above this layer in very shallow water at times, but we consider it a minor influence at this close to bed height (15 cm). Wave shear stress is estimated by (Hansen and Reidenbach, 2012):

$$\tau_w = 0.5 f_w \rho_w U_w^2 \text{ with } f_w = 0.04 \left( \frac{U_w T}{2\pi k_b} \right)^{-0.25}, \ U_w = 2\sqrt{u_w'^2 + v_w'^2}$$
(3)

where  $f_w$  is the wave friction factor;  $U_w$  is the significant wave orbital velocity; T is the significant wave period; and  $k_b$  is the roughness height

of the bottom, which is defined as  $2.5D_{50}$ .

#### 2.3.2. Sediment dynamics

The OBS sensor was calibrated post-deployment in the laboratory due to the difficulty of collecting water samples on the tidal flat during the observation. Water samples used for calibration were obtained at the high concentration fringe at the water line under low wave condition, thus the calibration was representative of fine-grained suspended sediment. The correlation coefficient  $\mathbb{R}^2$  of the laboratory calibration was 0.95 (data point N=26, figure not shown).

The LISST data have been checked before further processing, and low quality data with optical transmission < 15% were neglected (recommended by the manufacturer). These low quality data were mainly due to the occurrence of high SSC (> 0.8 g l<sup>-1</sup>). Mean floc size  $D_M$  was obtained from the volume concentration distribution measured by the LISST. The floc effective density  $\Delta \rho$  (i.e., bulk density less the water density) was determined by using results of the LISST and OBS, following Mikkelsen and Pejrup (2001):

$$\Delta \rho = \rho_f - \rho_w = \frac{M_f}{V_f} - \rho_w = \left(1 - \frac{\rho_w}{\rho_p}\right) \frac{M_p}{V_f} \tag{4}$$

where  $\rho_f$  is floc density,  $\rho_p$  is the primary particle density which is estimated to be about 2500 kg m<sup>-3</sup>, given a density of 2650 and 1300 kg m<sup>-3</sup> for mineral particulates and organic matter, respectively (Markussen and Andersen, 2013), and an organic matter content of 9% (mass ratio) determined by loss on ignition.  $M_f$  is the floc mass per unit volume,  $V_f$  indicates the floc volume concentration observed by LISST, and  $M_p$  is the SSC derived from calibrated OBS-3 + results.

The settling velocity of floc  $\omega_s$  was estimated by using Stokes' Law. When the particle Reynolds number Re =  $\omega_s D_M \rho_w / \mu > 1$ , indicating flocs fell beyond the viscous Reynolds region, a modified formula was applied to account for inertial drag during floc's settling (Winterwerp, 1998):

$$\omega_{s} = \frac{\Delta \rho g D_{M}^{2}}{18\mu} \text{ for } Re = \omega_{s} D_{M} \rho_{w} / \mu < 1.$$

$$\omega_{s} = \frac{\alpha}{18\beta} \frac{\Delta \rho g D_{M}^{2}}{\mu (1 + 0.15Re^{0.687})} \text{ for } Re = \omega_{s} D_{M} \rho_{w} / \mu > 1$$
(5)

where g is the acceleration due to gravity (9.8 m s $^{-2}$ ),  $\mu$  is the molecular viscosity of water (t=14 °C,  $\mu=1.17\times10^{-3}$  Pa s).  $\alpha$  and  $\beta$  are coefficients depending on the shape of particles. In this study, flocs were considered to be spherical particles with  $\alpha=1$  and  $\beta=1$ .

The topmost bed sediment ( $\sim 1$  cm thick layer) collected on April 29 was analyzed using a Mastersizer 2000 (measuring range 0.02–2000  $\mu m$ , reproducibility error < 3%) after  $H_2O_2$  and sodium metaphosphate treatment to remove organic matter and disaggregate flocs, respectively, and 15 min of sonification. Results showed that the median and mean grain size of the bed samples were 48.7 and 30.7  $\mu m$ , respectively, constituting of about 13% clay (< 4  $\mu m$ ), 46% silt (4–62  $\mu m$ ), 30% very fine sand (62–125  $\mu m$ ), and 11% fine sand (125–250  $\mu m$ ). Organic matter content of the bed sediment was determined through ignition at 450 °C for 6 h, and results showed that organic matter content of the surface bed sediment was about 9% ( $\pm$  1%).

#### 3. Results

#### 3.1. General time series

Time series of 25 days' hydrodynamics and SSC over the mudflat during tidal immersion are shown in Fig. 2. A storm was observed during the measurement period, i.e., the grey part between May 6 and 12. During stormy conditions, the mean wind speed was  $12.0~{\rm m~s^{-1}}$ , and wind directions were mainly in northeastward direction, i.e., from the main channel towards the flat (Fig. 2a). Wind speeds were much smaller during calm conditions, with a mean value of  $3.6~{\rm m~s^{-1}}$ . The significant wave height Hs was typically  $< 0.1~{\rm m}$  during calm weather, and increased significantly during the storm, reaching up to  $0.5~{\rm m}$  on May  $10~{\rm (Fig.~2b)}$ .

Fig. 2c shows the variation of water depth with a strong semidiurnal signal. The measurement period started during spring tides with a maximum water depth of approximately 4.5 m. Note that the storm occurred between neap tide (May 6-8) to middle tide, with the maximum water depth of about 3.8 m to 4.1 m. Variations of long- and cross-shore flow velocities at 15 cmab (u and v, respectively) are presented in Fig. 2d. Flood currents (positive *u*) were overall stronger than ebb currents (negative u). The maximum flood and ebb velocities were about 0.4 and 0.3 m s<sup>-1</sup>, respectively. Cross-shore currents ( $\nu$ ) mainly occurred in the off-shore direction during the ebb tides and were typically  $< 0.1 \text{ m s}^{-1}$ . During the storm (May 6–12), long-shore current velocities (u) were influenced by increased wind speed: the eastward currents (positive u) were observed for most of the time within tidal cycles. Off-shore currents more regularly occurred and lasted longer time around low water (LW) during the stormy conditions than those during calm conditions. The maximum off-shore currents up to  $\sim 0.2 \,\mathrm{m \ s^{-1}}$  were observed between May 10–11.

Variations of current-induced shear stress  $\tau_c$ , wave-induced  $\tau_w$ , and the total shear stress  $\tau_{cw}$  are presented in Fig. 2e. During calm weather, wave-induced shear stress was mainly below  $0.02\,\mathrm{N\,m}^{-2}$ , and the maximum current-induced shear stress was about  $0.3\,\mathrm{N\,m}^{-2}$ . Both  $\tau_c$  and  $\tau_w$  increased significantly during the stormy weather with the maximum values reaching 1.2 and  $1.0\,\mathrm{N\,m}^{-2}$ , respectively. The shear stress during storm approaches better the diurnal tidal signal while during calm periods it corresponds better with a quarter-diurnal signal.

It should be noted that as significant erosion occurred during the storm, the shear stresses might be underestimated a little in the end of the storm period compared to those in the beginning of the measurement due to the increase of distance between ADV sensor and bed surface.

Fig. 2f shows that SSC changed in a wide range between 0.01 and 4.0 g l  $^{-1}$  during this survey. Note that the maximum SSC before the storm (April 28 to May 6) was smaller than that after the storm, with nominal values of  $\sim$ 1.5 and 3.5 g l  $^{-1}$  for these two calm periods, respectively. Variations in shear stress as well as SSC within the tidal cycle under different weather conditions will be discussed later in Sections 3.3 and 3.4.

Fig. 2g shows the bed level variation reflecting the processes of erosion and deposition. Bed level remained stable during the calm conditions before the storm with  $\sim 3$  mm net erosion (not clear in the figure due to the large scale) during spring tides between April 29 and May 2, and a deposition of  $\sim 7$  mm in the following middle tides. During the storm, the bed eroded more quickly with bed level dropping incrementally at low waters and amounting to a net loss of  $\sim 110$  mm over six days. The most significant erosion of  $\sim 50$  mm occurred over two LW periods in two tidal cycles between May 10 and May 11. After the storm, a deposition of  $\sim 40$  mm was measured in a week between May 15 and 22. Note that the ADV was reset and the initial bed elevation was plotted as zero on May 15. Contrary to erosion process during the storm, deposition process after the storm was quite smooth.

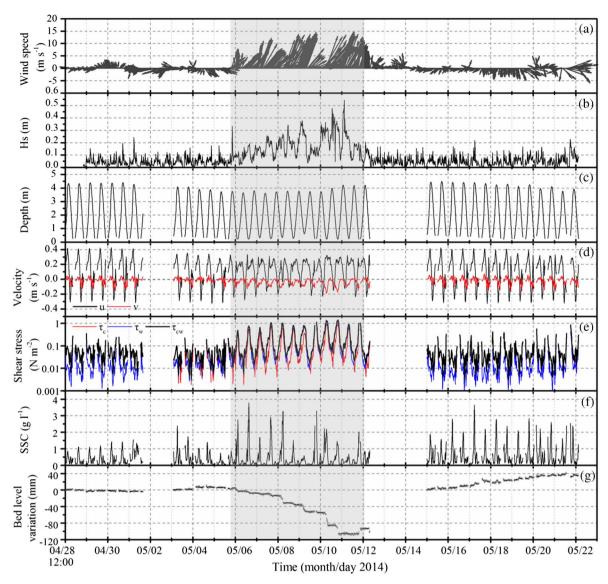
#### 3.2. In situ particle size distributions (PSDs)

Time series of in situ floc size distributions are presented in Fig. 3a as volume fractions of 32 groups of particles ranging from 2.5 to 500  $\mu$ m. The frequency of each size class is calculated by dividing the volume of each class by the total volume detected by the LISST. Two modes were observed in the PSDs, one was between  $\sim 80$ –200  $\mu$ m, and the other was around 400  $\mu$ m. Unlike the smaller mode, which could be found in nearly all the observation periods, the occurrence of the larger mode was not continuous but at regular intervals, related to flood-ebb tidal cycles. Fig. 3b shows the changes of mean floc size  $D_M$  and water depth.  $D_M$  ranged between  $\sim 50$ –200  $\mu$ m, and exhibited strong intratidal variations in phase with water depth. The variation of  $D_M$  during the stormy periods was periodic, increasing with an increase in water depth, resulting in larger and smaller  $D_M$  at around high water (HW) and LW, respectively. During the calm periods,  $D_M$  was more irregular, while large flocs still occurred around HW.

#### 3.3. Calm conditions pre- and post-storm

Fig. 4 shows typical data covering two tidal cycles (24 h) under preand post-storm periods, respectively. It was close to spring tide in April 28–29, with the maximum flood and ebb velocities values of  $\sim$  0.42 and 0.32 m s<sup>-1</sup>, respectively. The maximum flood and ebb velocities between May 19 and 20 were  $\sim 0.38$  and  $0.32 \, \mathrm{m \, s^{-1}}$ , respectively. Current velocities were controlled by tidal dynamics, and it was flood dominated with larger peak flood velocities and longer flood durations than ebb tides. The maximum flood velocity occurred about an hour before HW, after that flood velocity dropped quickly and inversed to ebb currents within 2 h. Bed shear stress  $\tau_{cw}$  varied between 0.01 and 0.25 N m<sup>-2</sup> under these two calm conditions. At the beginning and end of tidal immersion, large SSC ( $> 0.5 \,\mathrm{g}\,\mathrm{l}^{-1}$ ) were observed in shallow waters. The largest SSC in a tidal cycle was measured at about 1-2 h before HW, values were  $\sim 1.0 \, \mathrm{g} \, \mathrm{l}^{-1}$  before the storm and 2-3 times larger after the storm. The change of bed level was just within ~2-3 mm in a tidal cycle before the storm, with no clear erosion/deposition pattern. However, under the calm conditions after the storm, significant deposition of  $\sim$  4–5 mm was observed around HW, following a slight erosion in the ebb tide, and about 3 mm of net deposition was left per tide.

Fig. 4d shows the variations of mean floc size  $D_M$  and floc effective



**Fig. 2.** Time variations of (a) wind speed and direction; (b) significant wave height Hs; (c) water depth; (d) long- and cross-shore flow velocity u and v at 15 cmab, respectively; (e) current-induced  $τ_c$ , wave-induced  $τ_w$ , and total shear stress  $τ_{cw}$ , respectively; (f) suspended sediment concentration (SSC) at 15 cmab; and (g) bed level variation. Negative value indicates bed erosion, and the bed level variation was reset on May 15. The grey shaded area between May 6 and May 12 covers the stormy periods.

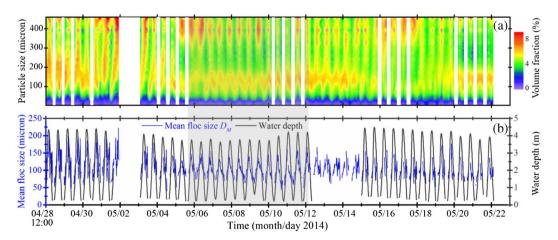


Fig. 3. Time evolution of (a) in situ floc size distribution, white columns cover periods without data around LW; (b) mean floc size  $D_M$  (blue line, the left y axis) and water depth (black line, the right y axis). The grey shaded area between May 6 and May 12 covers the storm period. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

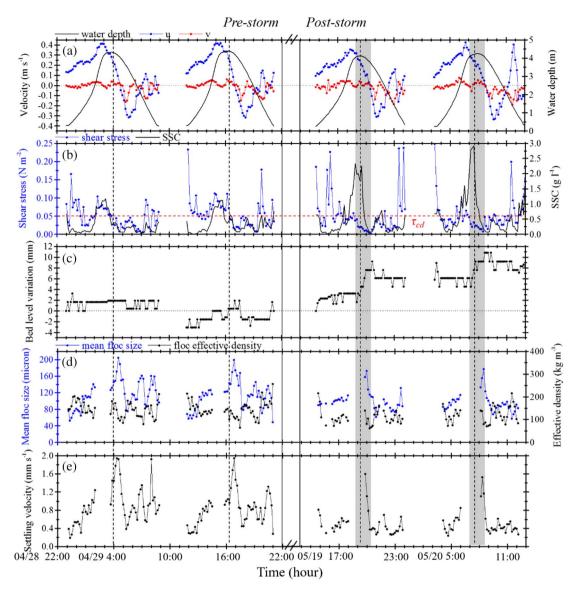


Fig. 4. Typical data under calm conditions pre- and post-storm on April 28–29 and May 19–20, respectively: (a) water depth (black line), long-shore velocity u (blue line), and cross-shore velocity v (red line); (b) bed shear stress  $\tau_{cw}$  (blue line) and suspended sediment concentration SSC (black line), the red dash line indicates the value of critical shear stress for deposition  $\tau_{cd}$ ; (c) bed level variation; (d) mean floc size  $D_M$  (blue line) and floc effective density  $\Delta \rho$  (black line); (e) floc settling velocity  $\omega_s$ . The four vertical dash lines correspond to HW, and the grey shaded areas cover the major deposition processes. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

density  $\Delta \rho$ , the gaps around HW were due to unreliable LISST results under high SSC. Floc size ranged from 50 to 200 µm before the storm, and the range decreased to 60–180 µm after the storm. The variation of  $D_M$  with tidal phase under these two calm periods was similar:  $D_M$  increased gradually from LW to HW and reached the peak value around HW slack, after that  $D_M$  decreased ~50% down to about 80 µm in 1 h. Then  $D_M$  fluctuated within 80–160 µm (pre-storm) and 80–120 µm (post-storm) over the next 4 h.  $\Delta \rho$  changed between 60 and 250 kg m  $^{-3}$  within the tidal cycle, and smaller effective densities usually corresponded to larger mean floc sizes. Floc settling velocity  $\omega_s$ , presented in Fig. 4e, varied between 0.2 and 2.0 mm s  $^{-1}$  and 0.2–1.6 mm s  $^{-1}$  before and after the storm, respectively, and followed a similar trend to  $D_M$  throughout a tidal cycle.

The typical in situ PSDs within a tidal cycle during the calm weather are presented in Fig. 5. The LISST derived sediment particle size distributions revealed varied unimodal and bimodal patterns at different tidal phases. It was found that in situ PSD in the beginning of the flood tide was similar to that of the bed sediment (Fig. 5a), with the mode being slightly coarser than the corresponding mode of the bed sediment ( $\sim$ 80 µm). As flood ebb continued, the peak of in situ PSD shifted

towards the coarser end, and another larger mode occurred when it came close to HW and around HWS (Fig. 5c and d). Soon after the HWS, the PSD became unimodal again and the peak shifted towards the finer end close to the peak of bed sediment, with the mean floc size decreased significantly from 189 to 77  $\mu$ m. Then the peak of PSD shifted between the coarser and finer part as mean floc size fluctuated in the late ebb tide. Note that there were raised tails at the coarser end of some distribution curves, which was due to the presence of particles beyond the measurement range of LISST (< 500  $\mu$ m). These particles with diameter > 500  $\mu$ m were likely to cause under-estimation of  $D_M$  to some degree. The effects of raising tails are minor under conditions like Fig. 5b and f, as the dominant portion of particles has been detected (Voulgaris and Meyers, 2004), while special attention should be paid around HWS.

#### 3.4. Stormy conditions

Fig. 6 presents typical stormy data from May 10 to 11 when the most significant erosion occurred. During this period, the average wind speed was  $15.3\,\mathrm{m\,s^{-1}}$ , and the onshore wind directions changed

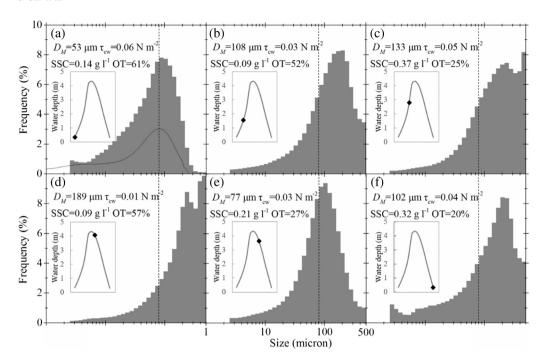


Fig. 5. Floc size distributions under different tidal phases during calm conditions on April 28–29. The black curve in (a) shows the dispersed grain size distribution of bed surface sediment, and the vertical dashed lines indicate the peak of the bed sediment distribution. OT indicates optical transmission over path of LISST.

between 230 and 250°. The wave activity was strong with the current velocity reaching  $\sim 0.35 \, \text{m s}^{-1}$  in shallow water and lasted until 2 h before HW. Off-shore currents (see red line in Fig. 6a) of  $\sim$  0.1-0.2 m s  $^{-1}$  also continuously occurred in shallow water. The combined shear stress  $\tau_{cw}$  ranged from about 0.04 to 1.5 N m<sup>-2</sup>, an order of magnitude larger than for the calm conditions. The largest shear stress occurred around LW, and decreased rapidly to about  $0.2 \,\mathrm{N\,m^{-2}}$  when the water depth was more than  $\sim 1 \,\mathrm{m}$ . During the stormy periods, SSC varied between 0.02 and 2.3 g l<sup>-1</sup>, with the maximum value occurring around LW and a smaller peak of SSC  $(\sim 0.5 \text{ g l}^{-1})$  was measured before HW in the tidal cycle.  $D_M$  increased from the minimum of  $60\,\mu m$  in shallow water to the maximum of 160 µm close to HW, and after that it decreased gradually with decreasing water depth. Relative large floc effective density over 200 kg m<sup>-3</sup> was measured in shallow water, and  $\Delta \rho$  decreased quickly to about 50 kg m<sup>-3</sup> in the beginning of the flood phase. Floc settling velocity in the stormy conditions was between 0.2 and 1.2 mm s<sup>-1</sup>, and the largest  $\omega_s$  was found about 1–2 h before the HW.

Fig. 7 shows the in situ PSDs within a tidal cycle during the stormy weather. It was found that the variations of PSDs were quite asymmetrical between flood and ebb tide. The peak of PSD shifted towards the coarser end during flood tide, then reversed to the finer end during ebb tide. The PSD in the beginning of flood resembled that in the end of ebb tide, with similar peak corresponding to the mode of the bed sediment (Fig. 7a and f).

In summary, large differences have been found in the hydrodynamics and sediment dynamics in storm/calm conditions. During the stormy periods, positive long-shore currents lasted longer in a tidal cycle, and off-shore currents around LW were more significant than those in calm periods. The maximum SSC as well as bed erosion occurred around LW during the storm, however, the maximum SSC and bed deposition (post-storm) in a tidal cycle under the calm conditions were observed around HW. Mean floc size  $D_M$  showed an overall increase with the increase of water depth for both storm and calm conditions, and it decreased gradually from HW to LW during the storm, while  $D_M$  dropped quickly and was more fluctuate after reaching the maximum around HW during the calm conditions.

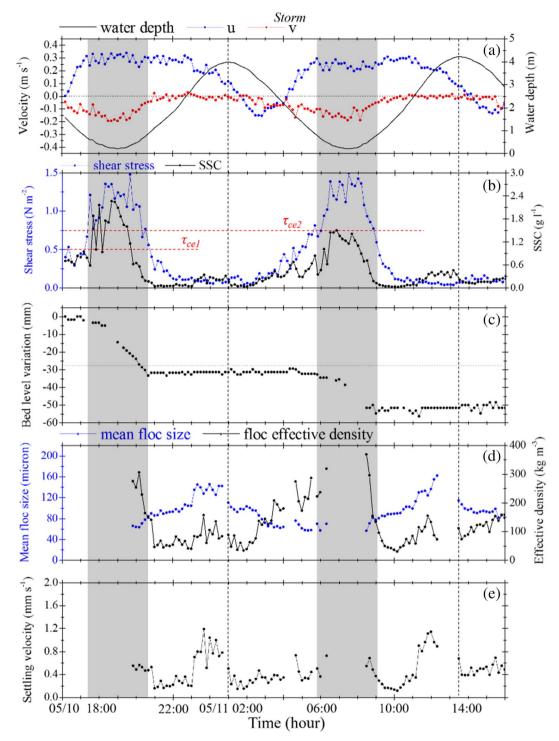
#### 4. Discussions

#### 4.1. Intra-tidal flocculation dynamics under different forcing conditions

Among many factors influencing flocculation, turbulence was expected to play the determining role in sediment flocculation in tidal cycles (Winterwerp, 1998; Dyer and Manning, 1999). Relationships between mean floc size  $D_M$ , shear stress  $\tau_{cw}$  and concentration SSC are presented in Fig. 8a and c. The measurements were split depending on weather condition (calm versus storm) and tidal phase (flood versus ebb). Considering the sediment dynamics following a strong storm were not quite typical, only the data before the storm were used as the representative of calm weather condition. The regressions of four conditions (calm flood/ebb and stormy flood/ebb) all illustrate negative correlations between  $D_M$  and shear stress, with regression parameters  $R^2 = 0.42$  and 0.36 for calm flood and ebb, respectively, and higher regression parameters of 0.71 and 0.65 were obtained for storm flood and ebb, respectively.

Although the pattern that floc size tended to decrease with the increase of shear stress were similar, a significant shift of the regression lines was found during flood and ebb phases under stormy period, indicating asymmetrical aggregation/break-up processes between flood and ebb tides. This asymmetry can be seen more clearly in Fig. 8d, which shows the typical variation of mean floc size within a tidal cycle. It can be interpreted from the asymmetry that floc sizes during flood are overall larger than those during ebb for the same shear stresses.

The asymmetrical flocculation behavior over the tide has been reported by a few authors and is attributed to the flocculation hysteresis effect, i.e. time scales for aggregation and break-up are different (e.g. Verney et al., 2011; Ramírez -Mendoza et al., 2016). In the laboratory research of Verney et al. (2011), they found that for a given shear rate, larger flocs were observed under increasing shear than those under decreasing shear, because the disruption of flocs was rapid once the shear force exceeded floc bond strength, while the aggregation process depended not only on moderate shear force, but also on collision efficiency and hence took longer time. However, the asymmetrical pattern observed in this case seemed to be contrary: flood tide (decreasing shear) showed larger flocs than ebb tide (increasing shear). This contrary result could be attributed to different environmental conditions under lab experiment and field survey. The same concentration of



**Fig. 6.** Typical data under stormy conditions on May 10–11: (a) water depth (black line), long-shore velocity u (blue line), and cross-shore velocity v (red line); (b) bed shear stress  $\tau_{cw}$  (blue line) and suspended sediment concentration SSC (black line), the red dash lines indicate the values of critical shear stresses for erosion:  $\tau_{ce1}$  and  $\tau_{ce2}$ ; (c) bed level variation; (d) mean floc size  $D_M$  (blue line) and floc effective density  $\Delta \rho$  (black line); (e) floc settling velocity  $\omega_s$ . The two vertical dash lines correspond to HW, and the grey shaded areas cover the major erosion processes. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

sediment was kept in suspension in the lab work of Verney et al. (2011), while significant resuspension (bed erosion) as well as settling took place during the storm in this study. As the bed sediment contains very fine (30%) and fine (11%) sand, the resuspension of bed sediment could change the constitutions of primary particles as well as sediment concentration thus affecting flocculation. The mixture of large-grain sand could also directly increase the particle size in suspension Meanwhile, Manning et al. (2010) found that sand could participate in flocculation and have important effects on the depositional behavior of mud/sand

mixtures under the presence of natural biological adhesives. It was found that the modal peak of in situ PSD was significantly larger than that of bed sediment, except at low water when the shear stress was the strongest and erosion happened (Fig. 7), this may partially support the occurrence of mixed mud and sand flocculation.

The settling of larger flocs, especially around HWS, could be another reason for smaller floc size during ebb tide. Note that in the end of HWS, floc sizes dropped rapidly for both calm and stormy conditions (Fig. 8b and d), and this could explain the large gap between

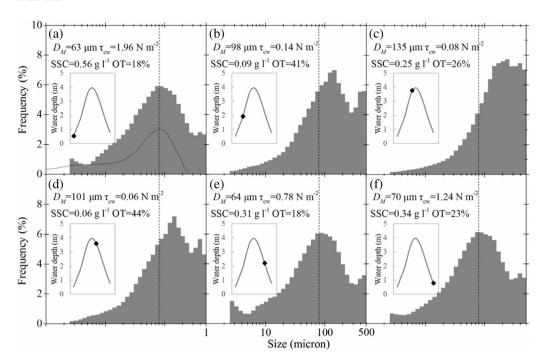


Fig. 7. Floc size distributions under different tidal phases during stormy conditions on May 10–11. The black curve in (a) shows the dispersed grain size distribution of bed surface sediment, and the vertical dashed lines indicate the peak of the bed sediment distribution. OT indicates optical transmission over path of LISST.

aggregation lines under low shear stress for calm conditions, although the asymmetry in the whole tidal cycle was not that clear. As mentioned before, floc sizes around HWS may be under-estimated to some degree due to the limited LISST measurement range, while the under-estimation in other tidal phases could be neglected, indicating that the

decreasing of floc size after HWS might be more significant than that presented here.  $\,$ 

According to the field survey, flood tide over the mudflat was characterized by a strong input of sediment, and large SSC in general, then settled around HW and was weekly resuspended during ebb tide.

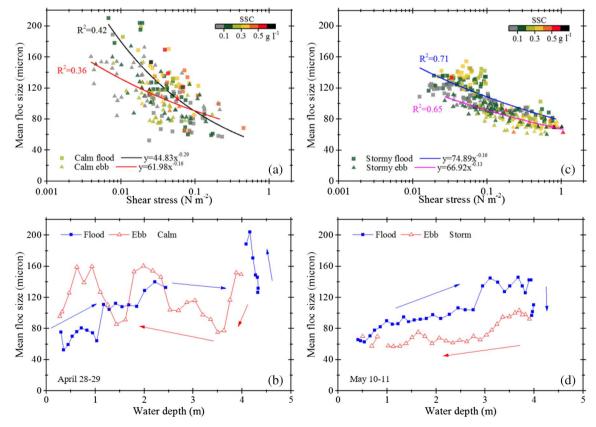


Fig. 8. (a)(c) Variation of mean floc size and shear stress under calm flood/ebb and stormy flood/ebb conditions, respectively; (b)(d) Typical variation of mean floc size with water depth in a tidal cycle under calm and stormy conditions on April 28–29 and May 10–11, respectively. In (a) and (c), solid lines are the regression results, and colour bar indicates corresponding suspended sediment concentration SSC. In (b) and (d), blue and red symbols represent flood and ebb tide, respectively. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

Differences of SSC between flood and ebb tides emphasized the effect of concentration on flocculation for similar turbulence levels. It was well illustrated in Fig. 8a and c that in the shear range of  $\sim 0.03–0.1$  N m  $^{-2}$ , mean floc sizes were overall larger with higher SSC, indicating that higher SSC may favor floc aggregation due to increased collision frequency. We could also scale the driving factors through Fig. 8a and c: turbulence is the dominant one, next SSC can modulate and enhance flocculation when turbulence decreases down.

# 4.2. Variation of floc effective density

Unlike the settling of non-cohesive sediment, the settling velocity of flocs not only relies on the particle size, but also on the floc structure. since the floc effective density is variable and related to the aggregation and break-up processes. Based on the self-similar fractal entities, Kranenburg (1994) proposed that:  $\Delta \rho \propto (\rho_p - \rho_w)(D_M/d)^{N_f} - 3$ , where d is the diameter of the primary particle and  $N_f$  is the floc fractal dimension, a mathematical parameter used as an indicator of particle morphology.  $N_f$  usually varied from 1.4 to 2.2 for large fragile flocs and strong flocs, respectively (Winterwerp, 1998). In the equation of Kranenburg (1994),  $N_f$  is a constant value over the size range for a certain simulation. However, some studies have noticed and used a variable fractal dimension with floc size in their simulations (e.g. Khelifa and Hill, 2006; Maggi, 2007; Kumar et al., 2010). The work of Khelifa and Hill (2006) suggested a quasi self-similar concept that  $N_f$ equals 3 for primary particles and then decreases with floc size in a power law function:  $N_f = 3(D_M/d)^{\beta}$ ,  $\beta = [\log(F_c/3)]/[\log(D_{fc}/d)]$ , where  $D_{fc}$  is a characteristic floc size, and  $F_c$  is the corresponding fractal dimension when floc size increases to  $D_{fc}$ .

Fig. 9 exhibits the correlation between floc effective density  $\Delta \rho$  and mean floc size  $D_M$ . It presents an overall decrease of effective density as mean floc size increases with  $R^2=0.34$  and 0.33 for calm and stormy conditions, respectively. However, it was found in the figure that floc effective density decreased more rapidly with mean floc size and resulted in lower effective density under stormy conditions than that under calm conditions. For the calm conditions, we found that applying the Kranenburg (1994) equation with  $N_f=2$  and  $d=10~\mu m$  was acceptable compared to the regression result, and it behaved better than the best fit using the Khelifa and Hill (2006) method. These results indicate that the floc fractal dimension may not be quite variable under

For the stormy conditions, however, neither the Kranenburg (1994) equation nor the Khelifa and Hill (2006) method could correctly simulate the observed dynamics. It was noted that  $\sim 16\%$  of the points

measured during the stormy conditions disagreed with the trend that effective density decreased with mean floc size and even showed a positive correlation between them. These points were measured in the late flood tide under mid to HW depth (> 2.5 m) when the turbulence was weak (< 0.1 N m<sup>-2</sup>), and flocs were large with mean floc sizes over 100 µm. From the simulation results in Fig. 9b, it can be seen that variations of effective density with floc size are sensitive to both characteristic fractal dimension  $F_c$  and primary particle size d, however they are usually defined as constant values in the simulations for simplification, and this may explain why the reverse regime cannot be reproduced. During the storm, bed sediment as well as organic matter were resuspended at low waters when erosions happened, leading to the change of floc constitutions and could alter floc properties. With the anticipation of more organic matter in the aggregation and break-up processes, floc effective densities could be expected to be lower for the same mean floc sizes and flocs more resilient to shear breaking (Mietta et al., 2009), moreover, the fractal dimension of floc may also become more variable. Note that an OBS sensor was less sensitive for sand, thus OBS-derived SSC may be underestimated during the stormy condition, especially around LW when the most significant erosion occurred and bed sand resuspended. Therefore, the estimated floc effective density would be overall underestimated to some degree as well, however, this overall underestimation would not have great effect on the tendency of the variation of floc effective density with floc size.

By using variable characteristic fractal dimension  $F_c$  and primary particle size d in the simulations, it was found that the reverse regime could be reproduced (Fig. 10). Although we are not sure about the detail processes in the field, we think the great variations of floc structure as well as primary particle property during stormy conditions may explain why the 'classic' fractal approach fails and why this inverse regime is not observed during calm conditions.

#### 4.3. Erosion and deposition processes under stormy and calm conditions

A few researches on the mudflat have concluded that the net import of suspended sediment usually happened in the form of repeated small imports in tidal cycles under the relative calm conditions, however, the net export was generally event controlled, such as in periods of strong on-shore wind (e.g. Christie et al., 1999; Andersen and Pejrup, 2001).

In this study, it was found that bed erosion during the storm occurred only around LW, when the shear stresses were the maximum and the off-shore velocities were significant. According to the bed level variation, the critical shear stress  $\tau_{ce}$  in the beginning of the storm was  $\sim 0.15$  N m<sup>-2</sup> (data not shown), and it increased to about 0.50 N m<sup>-2</sup>

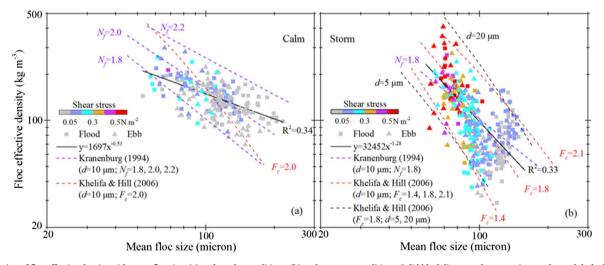


Fig. 9. Variation of floc effective density with mean floc size: (a) under calm conditions; (b) under stormy conditions. Solid black lines are the regression results, and dashed violet lines and dashed red (black) lines are results from the Kranenburg (1994) equation and the Khelifa and Hill (2006) method, respectively.  $D_{fc} = 100 \, \mu \text{m}$  in the simulations. Colour bar indicates corresponding shear stress. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

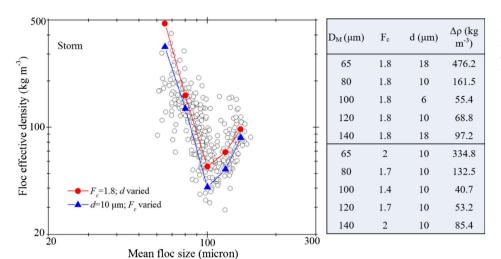


Fig. 10. Simulations of the variation of floc effective density with mean floc size in Khelifa and Hill (2006) method by using varied characteristic fractal dimension  $F_c$  and primary particle size d.  $D_{fc} = 100 \, \mu m$  in the simulations

on May 10 after 60 mm erosion,  $\tau_{ce}$  further increased to 0.75 N m<sup>-2</sup> in the end of the erosion period after another 30 mm erosion (Fig. 6). Large amounts of sediment were resuspended due to the high shear stresses around LW, then probably transported towards the channel by the continuous off-shore currents before settling back to the bed. Thus off-shore velocity played a vital role in the advection of sediment away from the tidal flat (Christie et al., 1999; Le Hir et al., 2000).

In the calm conditions before the storm, the bed level was relatively stable with the shear stress below  $\tau_{ce}$  (i.e. unable to erode the bed). A value of the critical shear stress for deposition  $\tau_{cd}$  was estimated to be  $\sim 0.05$  N m  $^{-2}$  based on the deposition processes that occurred after the storm (Fig. 4), meanwhile the values between 0.05 and 0.1 N m  $^{-2}$  were generally used in modelling studies (Whitehouse et al., 2000). The shear stress values before the storm were greater than  $\tau_{cd}$  before HW when the maximum SSC occurred, and this could be the reason why deposition did not happen before the storm.

After the storm, smooth deposition processes lead to a 36% (40 mm/110 mm) recovery in a week. This kind of quick recovery after a storm has also been reported by some authors (e.g. Christie et al., 1999; Andersen and Pejrup, 2001). In the research of Andersen and Pejrup (2001), they found that an equivalent of  $\sim\!40\%$  of the net annual deposition happened in five tidal cycles following a storm. As for the exact deposition periods during the tidal cycle, we found that they were

not fixed, with some occurring during HW and others between two tides (Fig. 11). Statistics show that about 15 mm ( $\sim$ 2–5 mm each time) of deposition occurred at low waters between May 16 and 19 just after the spring tide, accounting for 37.5% of the total deposition. The reasons for these depositions were not clear for now because of a lack of data in shallow waters, we could not explain why they only happened at four low waters, neither. The remaining deposition events were all measured around HW when the maximum SSC were observed. The occurrence of high SSC (>  $1.0 \,\mathrm{g}\,\mathrm{l}^{-1}$ ) around HW was attributed to tidal advection and the settling of sediment from the upper water column, as the variation of bed level showed no correlation with resuspension (Fig. 4b and c). Moreover, it was found that SSC around HW after the storm were about twice the values before the storm. This increase was expected because the nearby waters became more turbid after importing of large amount of sediment eroded from the tidal flat. The floc settling velocity within this period was estimated to be as high as 1.6 mm s<sup>-1</sup>, suggesting that only 47 min was required to settle over the full water depth of 4.5 m.

Deposition rate was estimated in two methods: (1) multiplying SSC and settling velocity of flocs; (2) multiplying bed level variation rate and sediment dry density ( $\rho_{dry} = 800 \text{ kg m}^{-3}$ , assuming the water content of 90%). Time series of hourly averaged deposition rates estimated from these two approaches are presented in Fig. 11. Their results

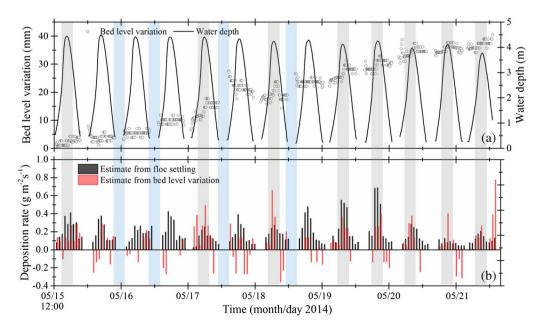


Fig. 11. Time series of (a) water depth and bed level variation; (b) deposition rate estimated from floc settling and bed level variation. The blue shaded areas cover bed accretion at low water, and the grey shaded areas cover bed accretion around high water. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

were in the same order of magnitude, with the maximum value of about 0.7 g m  $^{-2}$  s  $^{-1}$ . Large deposition rate (> 0.2 g m  $^{-2}$  s  $^{-1}$ ) usually occurred around HW, and the estimated deposition rate from floc settling around HW matched with the deposition rate estimated from bed level variation. However, in the early flood and the late ebb tides, these two results were quite different: floc settling flux was about 0.1 g m  $^{-2}$  s  $^{-1}$ , while the bed level variation was often close to 0 or even negative for a short time, indicating that deposition did not actually happened, which may be because the shear stresses were larger than  $\tau_{cd}$  in these periods.

#### 5. Conclusions

Variations of floc characteristics in tidal cycles and the effects of shear stress and SSC on aggregation and break-up processes were investigated under stormy and calm weather conditions over a muddy tidal flat.

Mean floc size changed between  $\sim$  50–200  $\mu$ m and exhibited strong temporal variations within a tidal cycle. Negative relationships between mean floc size and bed shear stress were found under both calm and stormy conditions, and asymmetries between flood and ebb phases were identified. This asymmetrical behavior was likely due to significant resuspension and settling processes in the field, and resulted in an overall larger mean floc size during the flood than during the ebb tide under the same shear stresses. Floc effective density showed an overall decrease with the increase of mean floc size, and two methods were used to simulate the correlation between them and were compared with the regression results. The simulation result with the Kranenburg (1994) equation by using a constant fractal dimension of 2 was acceptable during the calm conditions. While during the stormy conditions, a reverse regime of floc effective density increased with the increase of floc size was identified, when the floc size was larger than  $\sim 100 \, \mu m$ . This was likely due to the anticipation of resuspended bed sediment as well as organic matter in flocculation, and the observed dynamics could be reproduced by using variable characteristic fractal dimension or variable primary particle size in the Khelifa and Hill (2006) simulations.

Bed erosion during the storm only occurred around LW in a tidal cycle when the combined current-wave shear stress was maximum, and off-shore current played a significant role in the erosion process through transporting the resuspended sediment towards the channel within a short time. After the storm, about 40% of the erosion recovered within just one week, the fast settling of large flocs around HW plays significant role on the deposition process, resulting in  $\sim\!60\%$  of the total recovery.

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